

# Ultraviolet Chambers Based on Integrating Spheres for Use in Artificial Weathering

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## INTRODUCTION

Laboratory ultraviolet chambers (UV chambers) are the primary means for generating weathering data for a wide range of commercial products including coatings, elastomers, plastics, and polymeric composites.<sup>1</sup> Over the years, numerous technical improvements have been made in the design, construction, and control of these UV chambers. However, the reproducibility of exposure results obtained from these chambers has remained elusive.<sup>2-6</sup>

The reproducibility of UV exposure results is affected not only by variability in the material itself and its response to exposure, but also by *experimental* and *systematic* errors. Experimental errors and material variability, which are present in all experiments, are random in nature and can be compensated for through the use of proper experimental designs.

Systematic errors, on the other hand, are uncompensated, nonrandom sources of error which can strongly bias experimental results. Common sources of systematic bias associated with existing UV chambers include unnaturally high specimen temperatures, nonuniform spatial irradiance over the surface of a specimen, and temporal changes in exposure conditions. These errors can be minimized by standardizing test procedures, making changes in existing exposure equipment, or circumventing them through the use of alternate UV chamber designs. In this paper, an innovative UV chamber based on integrating sphere technology, which has the potential to mitigate a number of these systematic errors, is presented. In addition, it will be shown that the use of an integrating sphere-based UV chamber allows for added capabilities and greater flexibility in experimental design.

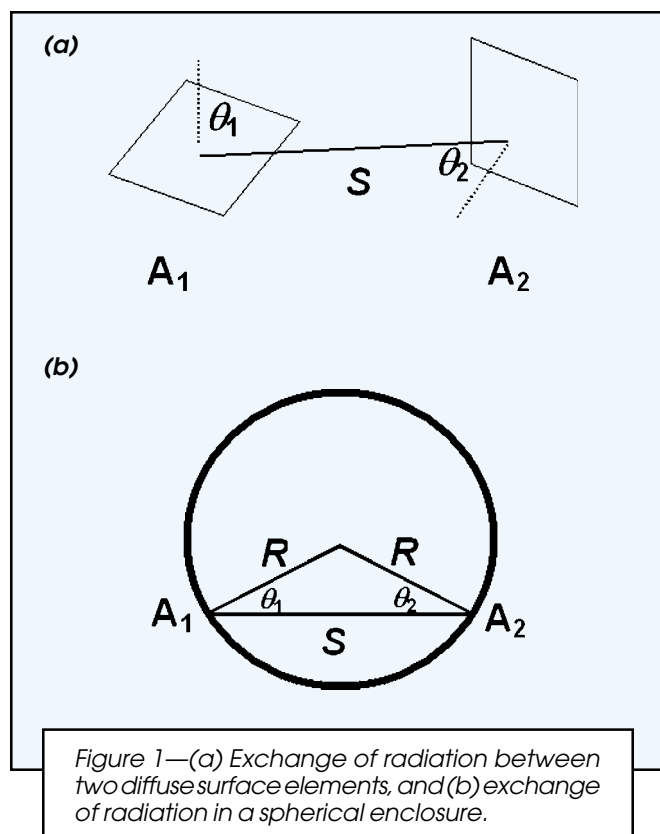


Laboratory ultraviolet (UV) chambers are widely used to obtain weathering data for a wide range of commercial polymer products including coatings, textiles, elastomers, plastics, and polymeric composites. Although numerous improvements have been made in the design of UV chambers over the last 80 years, the reproducibility of the exposure results from these chambers has remained elusive. This lack of reproducibility is attributed to systematic errors in their design, operation, and control which prevent direct comparisons of the performance of materials exposed in the same environment, comparisons of the performance of the same material exposed in different laboratories, and the comparison of field and laboratory results. This paper describes an innovative UV chamber design based on integrating sphere technology that greatly reduces the magnitude of these errors, as well as provides additional experimental capabilities.

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## CURRENT LABORATORY UV WEATHERING INSTRUMENTATION

Commercially available UV chambers began to appear circa 1920. Atlas Electric Devices\* introduced its carbon arc "Fade-O-Meter" in 1918; several years later, Nelson<sup>7</sup> published preliminary exposure results for a UV chamber using a mercury arc lamp in 1922, and Buttolph<sup>8</sup> patented several modifications to Nelson's UV chamber in 1924. UV chambers containing fluorescent lamps were introduced at a later date.

Numerous modifications in the early UV chamber designs have been made over the last 80 years. These modifications have been aimed at improving the repeatability and reproducibility of exposure results and include:

- (1) The development of UV sources with spectral distribution that more closely approximates the terrestrial solar spectrum,<sup>9-12</sup> and the use of filter combinations to remove radiation below 290 nm;
- (2) The employment of photopic sensors and feedback-control devices for monitoring and controlling temporal changes in the radiant power, thus improving temporal stability of the source;<sup>13-15</sup> and
- (3) The introduction of the three-tier exposure racks in xenon arc UV chambers, which served to improve the spatial irradiance uniformity over a specimen and between specimens.

\*Certain trade names and company products are mentioned in the text or identified in an illustration to adequately specify the experimental procedure and equipment used. In no case does such an identification imply recommendation or endorsement by the National Institute of Standards and Technology, nor does it imply that the products are necessarily the best available for the purpose.

These changes have greatly reduced the variability in exposure results, but they have not fully resolved issues related to the lack of reproducibility.<sup>5,6</sup>

## FACTORS AFFECTING REPRODUCIBILITY AND REPEATABILITY OF CURRENT UV CHAMBERS

Common sources of systematic error found in current UV chambers include unnatural exposure conditions (e.g., high specimen temperatures, nonterrestrial wavelengths), nonuniform irradiance over the dimensions of a specimen and among specimens, the inability to accurately and precisely measure ultraviolet radiation dose, and temporal changes in exposure conditions. Of these sources of error, unnatural exposure conditions and spatial irradiance nonuniformity have been the focus of NIST researchers as those which could be mitigated by the use of a novel integrating sphere-based UV chamber.

### Unnatural Exposure Conditions

The high current densities used in many arc lamps cause them to emit a substantial amount of energy in the visible and infrared regions.<sup>16,17</sup> In a typical UV chamber, the light source is situated in close proximity to the specimens, thus it has been observed that exposed specimen temperatures can approach 60°C.<sup>18,19</sup> These temperature levels are generally not consistently reached in most outdoor applications.

In the current commercial technologies, improved temperature control can be achieved by removing the primary source of thermal energy, visible and infrared radiation, while maintaining the photolytically effective ultraviolet radiation. This can be accomplished by introducing a heat controlling optical element (e.g., a dichroic mirror) between the light source and the specimen.

"Unnatural" chemistry in materials may also be induced by ultraviolet radiation with a wavelength less than 290 nm, which does not reach the earth's surface.<sup>20,21</sup> Efforts have been made by UV chamber manufacturers to eliminate these wavelengths by carefully researching light sources and utilizing cut-on filters. Although not a perfect match, certain grades of fluorescent lamps or xenon arc lamps equipped with borosilicate/borosilicate or CIRA/sodalime filters appear to be a close approximation to the solar spectrum.<sup>12</sup>

### Spatial Irradiance Uniformity

Ensuring spatial irradiance uniformity over the dimensions of a specimen and between specimens is a prime consideration in designing any optical system. Spatial uniformity is needed to determine that each specimen receives the same UV dosage. Spectral UV radiation dosage must be known in order to compare the performance of materials exposed in the laboratory and those exposed in the field.<sup>22,23</sup>

Spatial irradiance uniformity is difficult to attain in current UV chambers due, in part, to the large surface area over which uniformity must be controlled. Factors affecting irradiance uniformity include nonuniform emittance from the lamps, reflectance from the specimen and walls of the chamber, and physical limitations imposed by the optical system (e.g., the geometry of the light source,

dimensions of the specimens, and distance between the light source and the specimens).

## INTEGRATING SPHERE THEORY

The theory of integrating spheres, as well as their uses in a wide variety of applications, is well established.<sup>24-26</sup> An integrating sphere is a hollow spherical chamber with an inner surface coated with a diffusely reflecting, or *Lambertian*, coating. Light entering an integrating sphere undergoes multiple diffuse reflections at the interior surface, resulting in a uniform field of light within the sphere. This collected light can then serve as a means of measurement or as a source of uniform illumination. This latter function will be utilized in the novel UV weathering device. Integrating sphere theory has its origin in the theory of radiation exchange between diffuse surfaces.<sup>27</sup> Although the general theory can be complex, the symmetry of the sphere simplifies the analysis. Consider the exchange of radiation between two differential elements of diffuse Lambertian surfaces  $A_1$  and  $A_2$ , with areas  $dA_1$  and  $dA_2$  as shown in Figure 1(a). The fraction of the total flux leaving  $A_1$  ( $\Phi_{A_1}$ ) and arriving at  $A_2$  ( $\Phi_{A_2}$ ) is given by:

$$\frac{\Phi_{A_2}}{\Phi_{A_1}} = dF_{1-2} = \frac{\cos \theta_1 \cos \theta_2}{\pi S^2} dA_2 \quad (1)$$

where  $dF_{1-2}$  is known as the exchange factor. If these two surface elements are contained inside a diffuse sphere surface, and  $S = 2R \cos \theta_1 = 2R \cos \theta_2$ , as shown in Figure 1(b), then equation (1) becomes:

$$dF_{1-2} = \frac{dA_2}{4\pi R^2} \quad (2)$$



Figure 2—NIST 2 m integrating sphere, shown with UV light source.

Equation (2) is independent of the locations of the two elements and as well as the distance between the elements. This result is significant because it states that the fraction of flux received by  $A_2$  is the same for every other point on the sphere surface.

If the differential areas  $dA_1$  and  $dA_2$  become finite areas  $A_1$  and  $A_2$ , then equation (2) becomes:

$$dF_{1-2} = \frac{1}{4\pi R^2} \int_{A_2} dA_2 = \frac{A_2}{4\pi R^2} \quad (3)$$

Equation (3) is also independent of  $dA_1$ , allowing it to be expressed as:

$$dF_{1-2} = \frac{A_2}{4\pi R^2} = \frac{A_2}{A_s} \quad (4)$$

where  $A_s$  is the total surface area of the sphere. Thus, the fraction of energy received by  $A_2$  is proportional to the fraction of surface area that it takes up within the sphere.

The physical significance of the previous analysis is that every point on a sphere is equally illuminated by reflections from every other point. Theoretically, therefore, not only should the output intensity be uniform across the plane of an exit port, but every exit port should have the same spectral output as every other exit port. This property of integrating spheres will be exploited to produce an artificial UV weathering device with improved spatial irradiance uniformity. Thus, the use of an integrating sphere as a uniform UV radiation source can potentially resolve one of the major sources of systematic errors in current UV chamber design, that is, nonuniform irradiance across the dimensions of a specimen and from specimen to specimen.

The throughput, at a given port, of an integrating sphere with multiple ports is given by:

$$\frac{\Phi_o}{\Phi_i} = \frac{\rho f_e}{1 - \rho(1 - f_{tot})} \quad (5)$$

where  $\Phi_i$  is the input flux,  $\Phi_o$  is the output flux,  $\rho$  is the average sphere wall reflectance,  $f_e$  is the fraction of the sphere surface area taken up by the exit port of interest, and  $f_{tot}$  is the total fraction of the sphere surface area taken up by all of the exit ports. This equation assumes that no portion of the input flux is directly incident on any of the exit ports. It is generally recommended that  $f_{tot}$  be less than 5% if sphere output uniformity is critical. If the input flux is known, the output flux of an actual sphere can be calculated via equation (5).

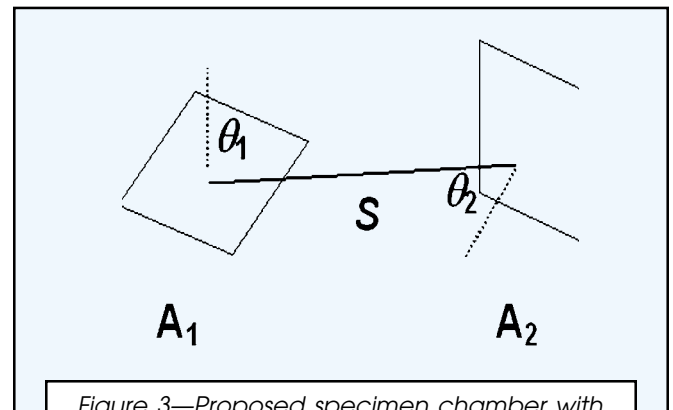
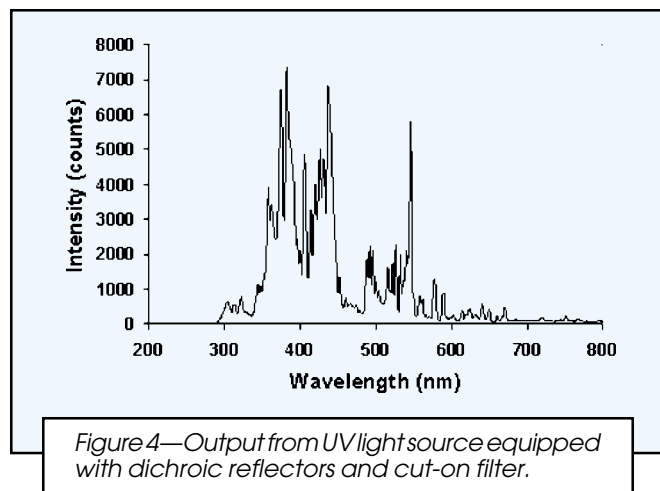
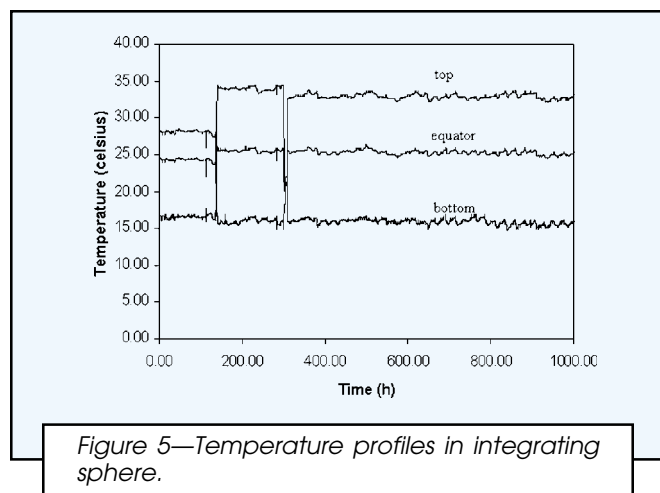


Figure 3—Proposed specimen chamber with capability for specimen loading.



In order for the previously mentioned equations to be correct and for an integrating sphere to be used successfully as an optical device, it is critical that the interior sphere surface scatter light in a Lambertian fashion over the wavelength region of interest. If the scattering is non-Lambertian, then the basic assumptions for the standard integrating sphere analysis are violated. The effects of non-Lambertian reflectance on the output of integrating spheres are presented by Hanssen.<sup>28</sup>

In the range of photolytically active wavelengths for polymeric materials, namely 290 nm to approximately 400 nm, materials with the highest Lambertian reflectance are based on barium sulfate powder or polytetrafluoroethylene (PTFE). The reflectance of pressed PTFE powder has been studied by Weidner and Hsia,<sup>28</sup> and was measured to be  $> 0.98$  in the region from 250 nm to 2000 nm. In recent years, a solid, machinable PTFE material has been developed having the high reflectance of the powder, but with greater durability and resistance to temperature, moisture, and corrosive chemicals. PTFE maintains its reflectance indefinitely under normal laboratory conditions if not contaminated with organic substances and does not need to be repacked or recoated.<sup>29</sup> In the event that reflectance does decrease over time due to surface contamination, the material can be sanded or vacuum baked<sup>30</sup> to regenerate its original reflectance.



## INTEGRATING SPHERE BASED UV CHAMBER

### Integrating Sphere

NIST researchers have developed a novel UV chamber based on a 2 m diameter integrating sphere and equipped with a high intensity UV light source, shown in Figure 2. The sphere is constructed from modular panels, allowing individual panels to be removed as needed for modification or repair. The exterior shell of the sphere is aluminum, and the interior surface is lined with PTFE panels. The sphere currently contains 32 11.2-cm diameter ports, and a 61-cm diameter top port to accommodate the UV light source.

### UV Light Source

The lamp system partnered with the 2 m sphere is a microwave-powered, electrodeless lamp system with an output that is rich in the region between 290 nm and 400 nm. A total of six lamps are utilized, symmetrically arranged around the top port of the sphere, with a calculated total output flux of 8400 W. A multiple lamp system, in contrast to a single lamp, allows the response of a material to various irradiance levels to be evaluated, thus providing opportunities to test the law of reciprocity. Because the light source is located outside the sphere, it is easily accessible for adjustments and repair. Dichroic reflectors in the lamp housings remove (80 to 90) % of the infrared and visible output from the lamps, and a cut-on filter is also installed in the optical path in order to remove radiation below 295 nm. In the event that wavelengths  $> 400$  nm are found to be critical in the photodegradation of certain materials, the dichroic reflectors can be replaced with conventional reflectors, thus retaining a greater proportion of the visible and infrared spectrum.

### Specimen Chambers

To study the durability of materials used in outdoor applications, it would be advantageous to uniformly irradiate specimens under a variety of exposure conditions. This could be accomplished by equipping each port with a specimen chamber in which temperature, relative humidity, mechanical loads, UV flux, and other factors can be independently controlled.

Because each chamber is independent of the others, a multiplicity of environmental conditions can be evaluated in a given experiment. While the UV irradiance would be identical between the ports, narrow band-pass filters or neutral density filters can be installed at the exit port to study the effect of a narrow wavelength region or to adjust the intensity, respectively. For instance, it would be possible to expose specimens at one exit port to 60°C, 95% relative humidity, polychromatic light; whereas, at another exit port, specimens could be exposed to 50°C, 95% relative humidity, and 290 nm radiation. Because the specimens at a given port are independent of all other specimens, and are also physically separated from the sphere and the lamp system, individual specimens can be entered into or taken out of test without disturbing the remaining specimens.

The capability to apply mechanical stresses, either cyclic or static, to the specimens while they are undergoing UV exposure can also be achieved, as shown in Figure 3.



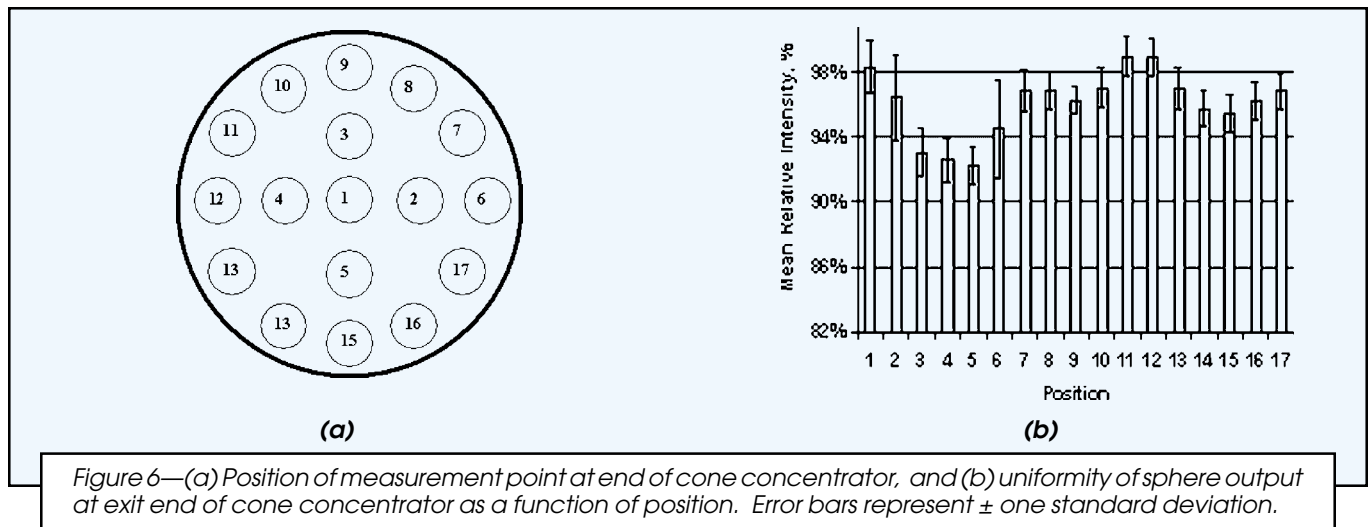


Figure 6—(a) Position of measurement point at end of cone concentrator, and (b) uniformity of sphere output at exit end of cone concentrator as a function of position. Error bars represent  $\pm$  one standard deviation.

Other unique exposure environments can also be created, including temperature cycling (including freeze/thaw), humidity cycling, and acid rain.

Conveyance and collimation of the highly uniform radiation from the sphere exit port to the previously described specimen chambers is accomplished with minimal loss of uniformity and intensity with the use of nonimaging optical devices. Such nonimaging optical devices are also referred to as compound parabolic concentrators, Winston cones, and cone concentrators, and are considered to be more efficient than conventional image-forming optics in concentrating and collecting light. These devices date back to the 1960s and were once used for solar collection; a detailed treatment of this subject is given by Welford and Winston.<sup>31</sup> In the application at hand, they will be used to collimate the diffuse output from the sphere exit port to a divergence angle of 20° and transfer it to the specimen surface.

## PRELIMINARY MEASUREMENTS

The output spectrum for the UV light source with the dichroic reflectors and cut-on filters in place is shown in Figure 4. It can be seen that output below 290 nm is virtually non-existent. While the output spectrum of this particular UV light source does not closely approximate natural sunlight, it is anticipated that the integrating sphere-based weathering device will be utilized in the context of a reliability-based approach to UV weathering proposed by Martin et al.<sup>32</sup> In this approach, the main concern is the spectral photoresponse of the materials undergoing exposure, not the polychromatic photoresponse; thus, matching of the solar spectrum is not critical. However, the design of the sphere system does allow for the use of alternative UV sources, such as xenon arc or fluorescent UV lamps.

Spectral measurements of the UV light source output were taken as a function of time, using a UV-visible spectrometer equipped with a collection sphere. The coefficient of variation for 700 independent spectra taken over every half hour for approximately 500 hr was found to be on the order of 1%. These measurements are routinely taken during the time that the UV light source is in operation, and are used to quantitatively assess the quality of

the UV output, which may be affected by changes not only in the lamps themselves, but in the transmittance or reflectance of any material in the optical path. This includes the reflectance of the dichroic elements, the sphere wall, and the interior of the cone concentrator, and the transmittance of the cut-on filter.

The sphere system is heavily instrumented with thermocouples to ensure that overheating of the sphere does not occur. Temperature profiles as a function of time at various positions in the sphere are shown in Figure 5. In general, temperatures are quite stable and do not exceed 35°C.

UV-visible measurements were taken at 17 points [illustrated in Figure 6(a)] at the output end of the cone concentrators with all six lamps running at 100% power. A representative uniformity profile is shown in Figure 6(b), revealing that the uniformity over the measured points within the exposure area is 92% or better. Also, Figure 7 shows that UV-visible spectra taken at the center point of 14 different cone concentrators are virtually nondistinguishable. The data from this series of measurements leads to the conclusion that both the intra-port uniformity and inter-port irradiance uniformity of the integrating sphere output are high.

## CONCLUSIONS

UV chambers play an important role in comparing or predicting the performance of polymeric construction materials and determining the effect of different weathering factors on the performance of a construction material. Although significant modifications have been made in current UV chamber designs, controlling the systematic errors and thus the reproducibility of exposure experiments using these chambers has remained elusive. An integrating sphere UV chamber design is being developed which appears to be capable of mitigating known sources of systematic errors.

The improvements offered by an integrating sphere UV chamber over conventional weathering instrumentation are summarized as follows:

1. **SPATIAL IRRADIANCE UNIFORMITY:** As a uniform radiation source, an integrating sphere is capable of minimizing

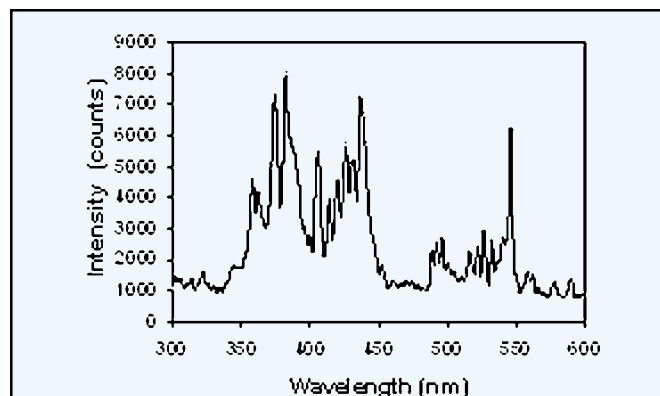


Figure 7—Sphere output taken at the center points of 14 non-equatorial ports, all spectra superimposed.

errors due to nonuniform irradiance over the dimensions of a specimen and from specimen-to-specimen. Spatial irradiance uniformity does not depend on the light source, the age of the light source, or batch-to-batch variability, but, instead, it is controlled by the physics of integrating spheres.

**2. REMOVAL OF RADIATION BELOW 290 NM:** By positioning a cut-off filter after the dichroic mirror, radiation below 290 nm can be removed from the radiant flux. Moreover, interference or cut-off filters can be positioned in front of each specimen so that each specimen can be uniquely irradiated using any combination of wavelengths.

**3. REMOVAL OF VISIBLE AND INFRARED RADIATION FROM THE RADIANT FLUX:** High specimen exposure temperatures can be minimized by removing most of the visible and infrared portions of the radiant energy flux emitted by the light source prior to entering the sphere. By removing most of the visible and infrared radiation emitted by the light, the temperature within the chamber can easily be maintained at slightly above room temperature.

**4. SIMPLICITY IN DESIGN AND EASY ACCESSIBILITY TO THE LIGHT SOURCE, EXPOSURE CELLS AND SPECIMENS:** The light source, exposure cells, and specimens are located on the exterior of the integrating sphere and, thus, they are readily accessible even while an experiment is in progress.

**5. EXPERIMENTAL FLEXIBILITY:** Finally, use of an integrating sphere provides the opportunity to simultaneously and independently expose a multiplicity of specimens each to its own exposure environment. This can be achieved by positioning specimens in individual exposure cells and uniformly irradiating the specimens by projecting the output from the exit ports with the use of non-imaging optical devices. The environmental and operating conditions within each exposure cell can be uniquely selected.

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